### Application Examples

#### Introduction
Optocouplers are used to isolate signals for protection and safety between a safe and a potentially hazardous or electrically noisy environment. The interfacing of the optocoupler between digital or analogue signals need to be designed correctly for proper protection. The following examples help in this area by using DC and AC input phototransistor optocouplers.

#### Optocouplers in IC Logic Design
To interface with TTL logic circuits, Vishay offers a wide range of 4 pin and 6 pin optocoupler series such as the CNY17x, SFH61xA, TCET110x, or K817P family.

- **a)** Supply voltage: \( V_{CC} = 5 \text{ V} \)
- **b)** Operation temperature range: \(-20 \degree C \) to \(+60 \degree C\)
- **c)** Service life of application: 10 years

**Example 1**
Phototransistor wired to emitter resistor.

For simplicity, a typical CTR value of 100 % at \( I_F = 10 \text{ mA} \) is selected. Within the temperature range of \(-20 \degree C \) to \(+60 \degree C\) the CTR undergoes change between +12 % and −17 %. The −17 % reduction is critical as applied to functioning of the circuit.

Assuming a 10-year service life period of the interface circuit, allowance needs to be made for additional CTR reduction of approximately 20 % on account of degradation. Making an additional tolerance allowance of approximately −25 % for the CTR will result in a safe minimum value of approximately 50 %.

\[
\text{CTR}_{\text{min}} = 100 \% \times (0.83) \times (0.80) \times (0.75) = 49.8 \%
\]

For a defined low state at the output of the optocoupler the voltage \( V_L \) at \( R_L \) must be \( V_{IL} \leq 0.8 \text{ V} \) and current \( I_{IL} \) (\( I_{IL\text{max}} = 1.6 \text{ mA} \)) must be capable of flowing through \( R_L \) from the TTL input.

Owing to the phototransistor in this case being blocked at the output of the optocoupler and \( I_{CEO} \) maximum 200 nA (at approximately 60 °C), \( I_L - I_{IL} \) setting can proceed practically without any error.

This results in the following maximum value of \( R_L \):

\[
R_L < \frac{V_{IL}}{I_{IL}} = \frac{0.8 \text{ V}}{1.6 \text{ mA}} = 500 \Omega
\]

A voltage \( V_L \) at \( R_L \) resistor of \( V_{IH} \geq 2 \text{ V} \) is necessary in order to attain a safe high state at the output. This needs to be generated by the collector current \( I_C \) of the phototransistor.

In the case of the TTL output at the input of the optocoupler the current should remain \( I_{OL} \leq 16 \text{ mA} \). The CTR value of 50 % results in maximum output current \( I_C \) for the optocoupler of 8 mA.

With \( I_L = I_C + I_{IH} \) and \( I_{IH} \) for standard TTL being maximum 40 µA, \( I_L = I_C \) can be assumed without any essential error.

This allows the minimum value to be determined for \( R_L \):

\[
R_L > \frac{V_{IH}}{I_L} = \frac{2 \text{ V}}{8 \text{ mA}} = 250 \Omega
\]

If for example \( R_L = 390 \Omega \) is selected and 20 % safety is computed to the minimum \( V_{IH} \) in respect of the high state \( (V_{IH} + V_{IH} \times 20 \% = 2.4 \text{ V}) \), this will then permit...
\[ I_C = I_L \geq \frac{2.4V}{390\Omega} = 6.15\ mA \]

\[ \Rightarrow I_f > \frac{6.15\ mA}{CTR} = 12.3\ mA \]

With \( V_F = 1.2\ V \) (the forward voltage of the IR diode) and \( V_{OL} \leq 0.4\ V \) for the TTL output follows

\[ R_V > \frac{V_{CC} - V_F - V_{OL}}{12.3\ mA} = 276\ \Omega \]

The TTL interface with the optocoupler is able to transmit signals having a frequency of \( > 50\ kHz \) or a transmission rate of \( \geq 100\ kbit/s \).

In the same way, the optocoupler can interface with other logic circuits, e.g., LSTTL or HCMOS, HCTMOS components. All that needs to be done is to work the corresponding limit values \( V_{IH}, V_{OH}, I_{IL}, I_{OL} \), etc., into the computation for the relevant family.

If use is made of LSTTL or HCTMOS components this will also bring about an essential reduction in current consumption.

**Example 2:**
Phototransistor wired to collector resistor

![Diagram of phototransistor circuit](image)

The CTR is determined applying the same calculation – 50% – as that given in example 1. In this example dimensioning of the interface is launched from the high state at the output of the optocoupler.

In the high state a non-operate current of the \( I_{IH} \) – of maximum 40 \( \mu A \) – may flow in the TTL input. If \( R_L \) selection is too high, the entire non-operate current \( = I_{CEO} + I_{IH} \) may produce such a voltage drop through the \( R_L \) that the critical \( V_{IH} \) voltage (minimum = 2 V), is not attained.

\[ R_L < \frac{V_{CC} - V_{IH}}{I_{CEO} + I_{IH}} = 5V - 2V \approx \frac{40,2\ \mu A}{40,2\ \mu A} = 74,6\ k\Omega \]

or if another \( + 20\% \) safety is added to the \( V_{IH} \) voltage,

\[ R_L < \frac{V_{CC} - (V_{IH} + V_{IH} \times 20/100)}{I_{CEO} + I_{IH}} = 5V - 2.4V \approx \frac{40,2\ \mu A}{40,2\ \mu A} = 64,7\ k\Omega \]

For calculating the smallest usable \( R_L \)-value \( I_{C_{max}} = 8\ mA \) is assumed as in example 1 and use is made of the low state of the optocoupler output. In this circuit the current \( I_{IL} \) of the TTL input flows through the phototransistor in such a way that the following applies: \( I_C = I_L + I_{IL} \).

This results in the following:

\[ R_L > \frac{V_{CC} - V_{IL}}{I_{C_{max}} - I_{IL}} = \frac{5V - 0.8V}{6,4\ mA} = 656\ \Omega \]

To select the value for \( R_L \) the following should be observed.

Proceeding from the voltage \( V_{IL} = 0.8\ V \) the phototransistor is on the limits of saturation.

Owing to the voltage \( V_{CE} \) being relatively unstable in this state, \( V_{CE} \) should be selected in such a way that the phototransistor is in full saturation.

From the diagram \( V_{CESat} \) vs. \( I_C \) in any given 4 pin or 6 pin phototransistor data sheet, CTR reduced by 50% and for \( I_C < 5\ mA \) follows \( V_{CESat} < 0.5\ V \).
IC\textsubscript{max} is now reduced to approximately 4 mA and for the minimum \( R_L \) follows,

\[
R_L > \frac{V_{CC} - V_{CESat}}{4mA - 1.6mA} = \frac{5V - 0.5V}{2.4mA} = 1875\Omega
\]

If a suitable value is selected for the resistor \( R_L \) it is possible to determine \( R_V \) at the input.

Example for \( R_L = 5.1 \text{ k}\Omega \) follows

\[
I_L = \frac{V_{CC} - V_{CESat}}{R_L} = \frac{5.5V}{5.1\text{k}\Omega} = 1.08\text{mA}
\]

\[
I_C = I_{IL} + I_L = 2.68 \text{ mA}
\]

and with CTR = 25\% \( I_F = I_C / \text{CTR} = 10.72 \text{ mA} \)

\[
R_V = \frac{V_{CC} - V_F - V_{OL}}{10.72\text{mA}} = 317\Omega, \; R_V = 330\Omega
\]

This interface circuit can be used for transmission rates of up to about 28 kbit/s The fact that considerably lower transmission rates are possible here compared with the circuit given in example 1 is partly due to the saturation state of the phototransistor and to a large extent to the higher value required for \( R_L \).

**Example 3:**

Here are other circuit configurations to interface with TTL circuit, specifically the 7400 family.

**TTL Active Level Low (7400)**

![Diagram](image1)

Note: Best method if negative supply is available.

![Diagram](image2)

Note: Requires 10 mA from transistor and sacrifices noise margin.

![Diagram](image3)

Note: High sensitivity but sacrifices noise margin. Needs extra parts.

![Diagram](image4)

Note: Extra parts cost but high sensitivity.

It is more difficult to operate into TTL gates in the active level high configuration. Some possible methods are as follows:
Input Driving Circuits
The input side of the optocoupler has an emitter characteristic as shown.

There are obviously many other ways to drive the device with logic signals, but a majority can be met with the above circuits. All provide 10 mA into the LED giving 2 mA minimum out of the phototransistor. The 1 V diode knee and its high capacitance (typically 100 pF), provides good noise immunity. The rise time and propagation delay can be reduced by biasing the diode on to perhaps 1 mA forward current, but the noise performance will be increased.

The forward current must be controlled to provide the desired operating condition.
The input can be conveniently driven by integrated circuit logic elements in a number of different ways.
AC Input Compatible Optocoupler

Introduction
With the rapid penetration and diversification of electronic systems, demand for optocouplers is strengthening. Most popular are products featuring compact design, low cost, and high added value. To meet the market needs, Vishay is expanding the optocoupler. This application note focuses on optocouplers compatible with AC input, and covers configuration, principles of operation, and application examples.

Configuration (Internal PIN Connection Diagram)

Figure 1 shows the internal pin connection of a 4-pin AC input SFH620A-x optocoupler TCET1600, K814P Series, and Figure 2, of a 4-pin DC input optocoupler TCET1100, SFH61xA-x, and K817P Series. The main difference is that the AC input optocouplers incorporates an input circuit with two Emitters connected in reverse parallel. In the DC input optocoupler one Emitter is connected in the input circuit so that the Emitter emits light to provide a signal when a current flows in one direction (1→2 in Figure 1) (one-direction input type). However, in the configuration shown in Figure 2, when a current flows in direction 1 to 2, Emitter1 emits light to send a signal, and when it flows from 2 to 1, Emitter 2 emits light to send a signal (bidirectional input type). Namely, even if the voltage level between 1 and 2 varies, and the positive and negative polarities are changed, either of two Emitters emits light to send a signal. This means that the one-direction input optocoupler permits DC input only, while the bidirectional input type permits AC input as well. The next section describes the status of output signals when V_{ac} power is directly input to an AC input compatible optocoupler via a current limit resistor.

Example 1: AC–DC converter
Example 2: Detection of a telephone bell signal

Figure 4. Conventional optocoupler (one-direction input)
(Full-wave rectification by means of diode bridge)

Example 3: Sequencer circuit input section

Figure 6. Conventional optocoupler (one-direction input)
(rectified by CR circuit)

Figure 5. AC input compatible optocoupler (bidirectional input)

Figure 7. AC input compatible optocoupler (bidirectional input)

Figure 8. Conventional optocoupler (one-direction input)
(Full-wave rectified by diode bridge)
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Programmable Logic Controller Example

Purpose: in–out interface